

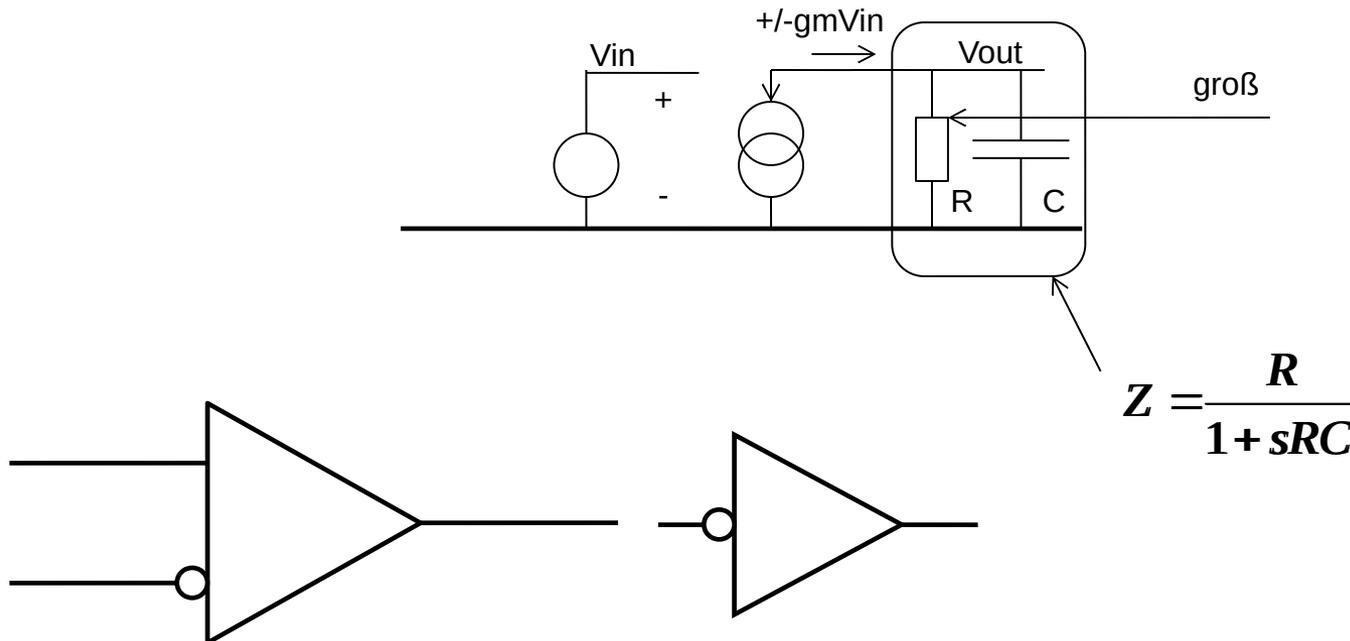
Verstärker mit zwei Stufen

Ausgangsstufen

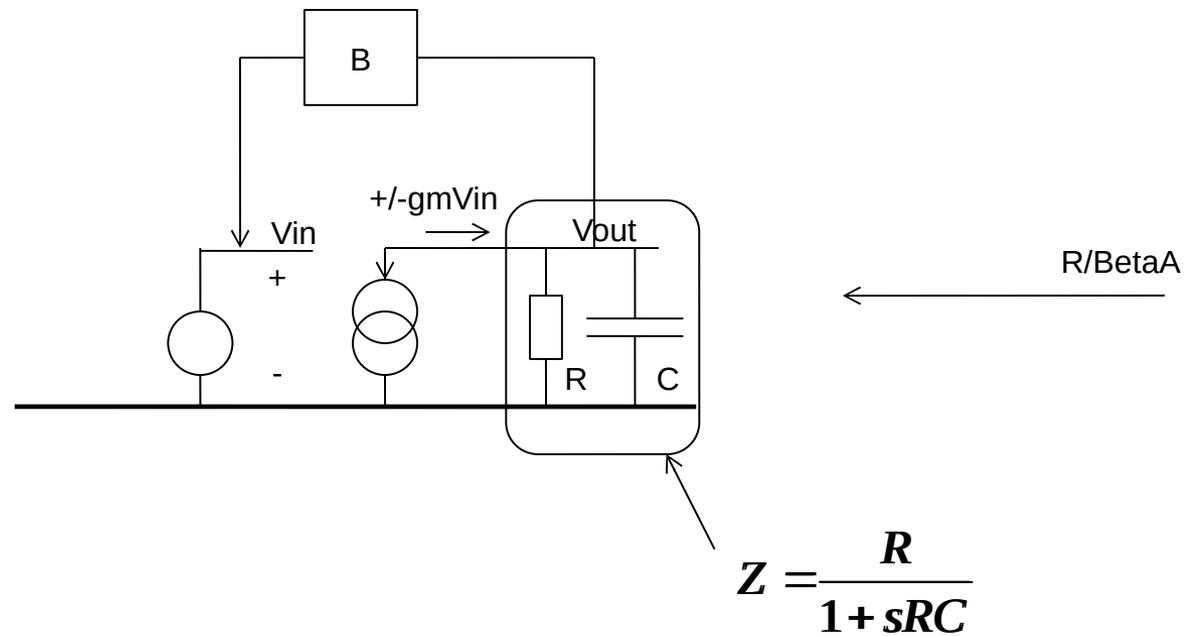
Source-Follower, Common-Source

Einstufiger Verstärker

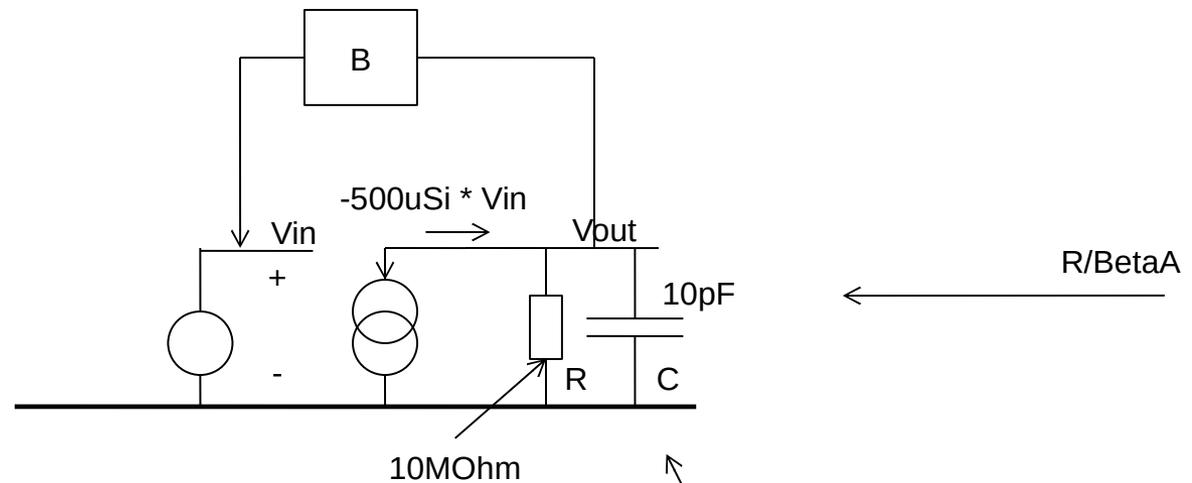
- Einstufige Verstärker
- U-I Konverter, Z_{out}
- Nachteil R_{out} groß



- $R_{out_fb} < R_{out}$



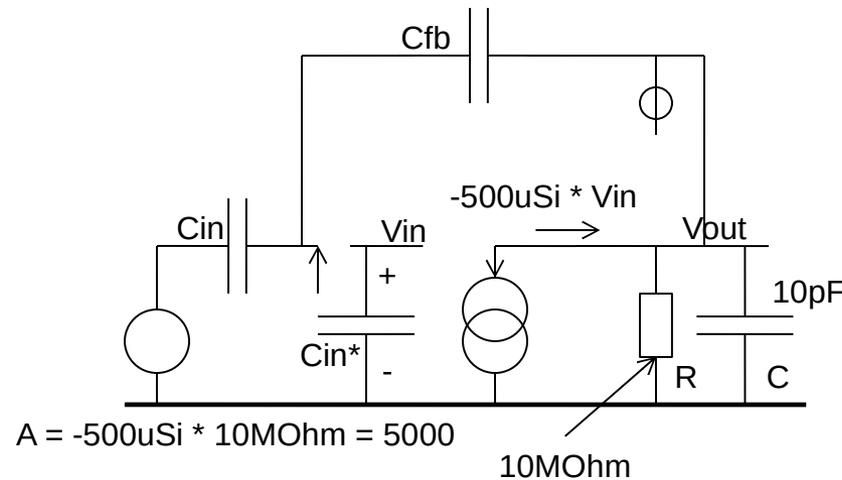
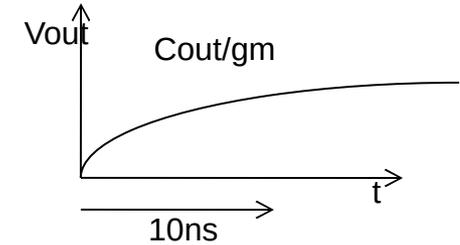
- Beispiel
- $A_{fb} = 100$
- $A_{ol} = 5000$



$$A = -500\mu\text{Si} * 10\text{M}\Omega = 5000$$

$$Z = \frac{R}{1 + sRC}$$

• ...



$$T_{fb} = C_{out} R_{out} / \text{Beta} A_{ol} = C_{out} R_{out} / \text{Beta} g_m R_{out} = C_{out} / \text{Beta} g_m$$

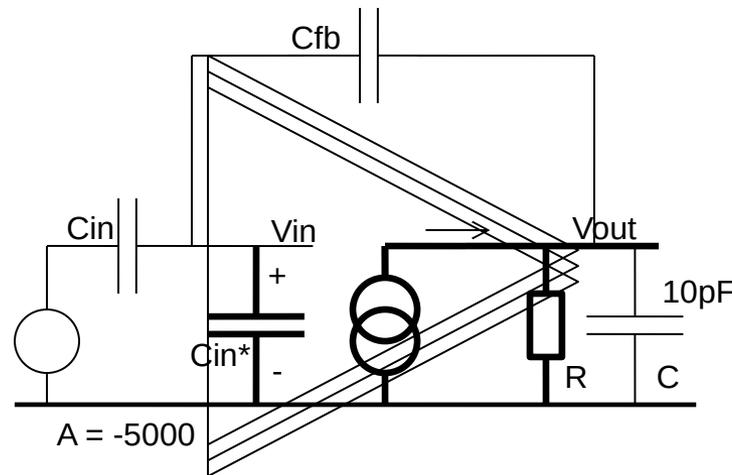
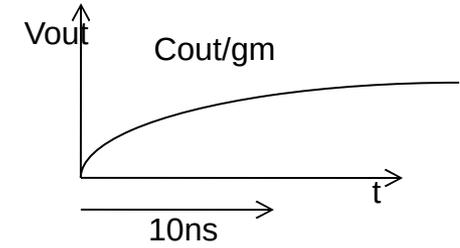
$$\text{Beta} = C_{fb} / (C_{fb} + C_{in} + C_{in}^*)$$

$$A_{fb} = -A_{in} / \text{Beta} = -C_{in} / C_{fb} \sim -1 / \text{Beta}$$

$$\text{Beta} \sim -1 / A_{fb} \Rightarrow \text{Beta} \sim 0.01 \quad \text{Falls } C_{in}^*, C_{fb} \ll C_{in}$$

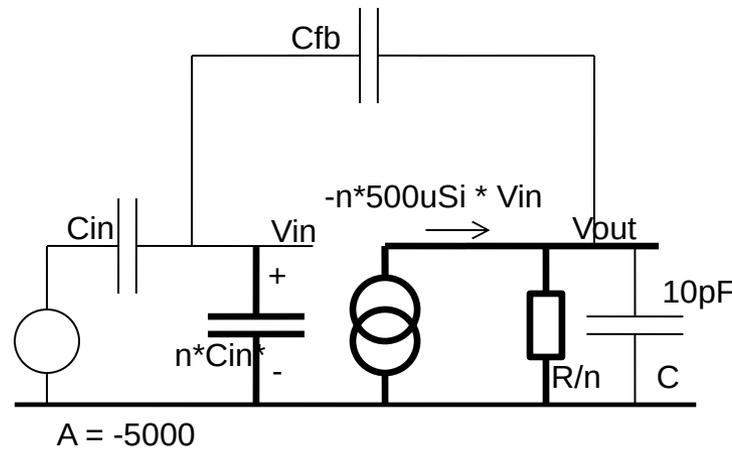
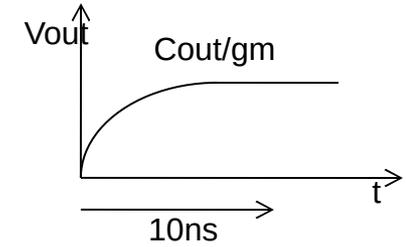
$$T_{fb} \sim C_{out} / 0.01 g_m \sim 100 \cdot 10\text{pF} / 500\mu\text{Si} = 2000\text{ns}$$

• ...



← $R/\beta A$

• ...



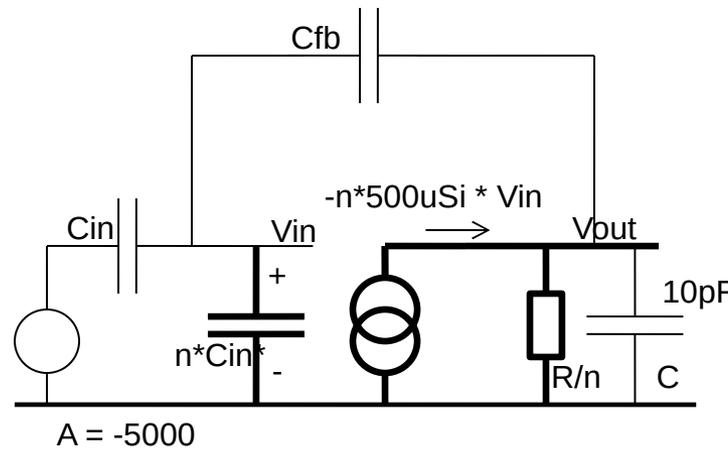
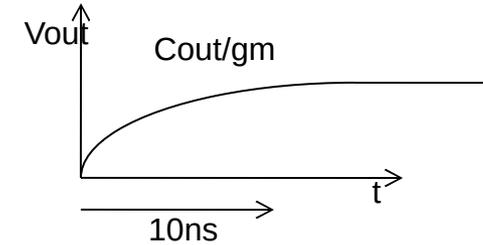
$\leftarrow R/\text{Beta}A$

$$T_{fb} = C_{out} R_{out}/n / \text{Beta} A_{ol}^* = C_{out} / \text{Beta} n^*g_m$$

$$N=200 \rightarrow T_{fb} = 10\text{ns.}$$

∞

• ...



$$T_{fb} = C_{out} R_{out}/n / \beta A_{ol} = C_{out} / \beta n g_m$$

$$N=200 \rightarrow T_{fb} = 10\text{ns.}$$

$$C_{in}^* = 200 * 20\text{f} = 4\text{pF.}$$

$$\text{Falls } C_{in} \sim C_{in}^* \quad \beta = C_{fb}/(C_{fb} + C_{in} + C_{in}^*) \ll 1/A_{fb} = 0.01$$

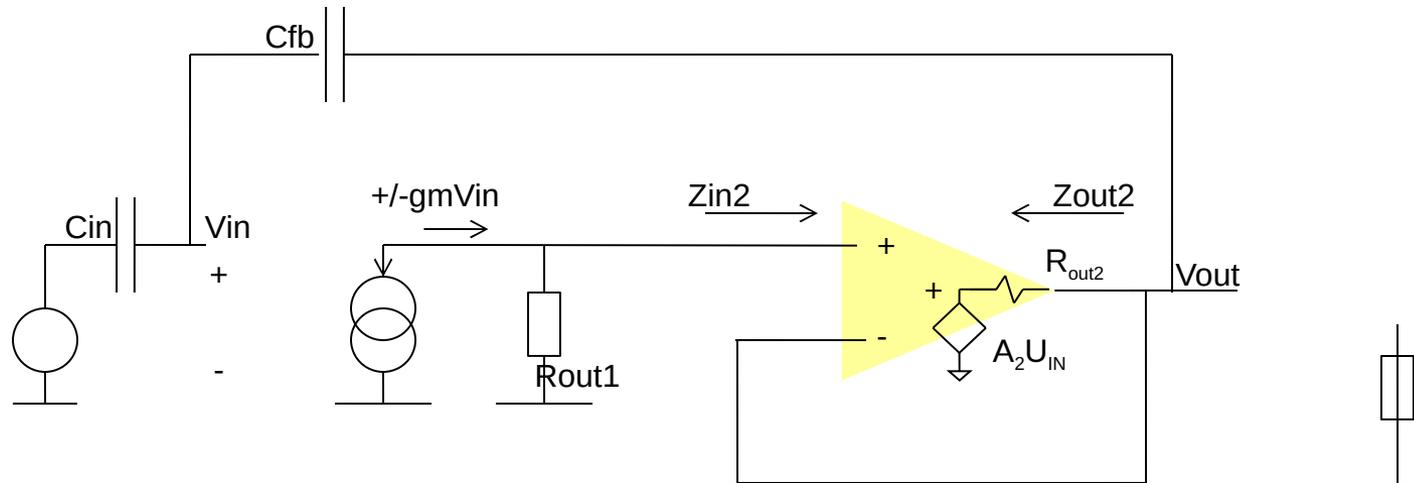
$$T_{fb} > 10\text{ns.}$$

←t

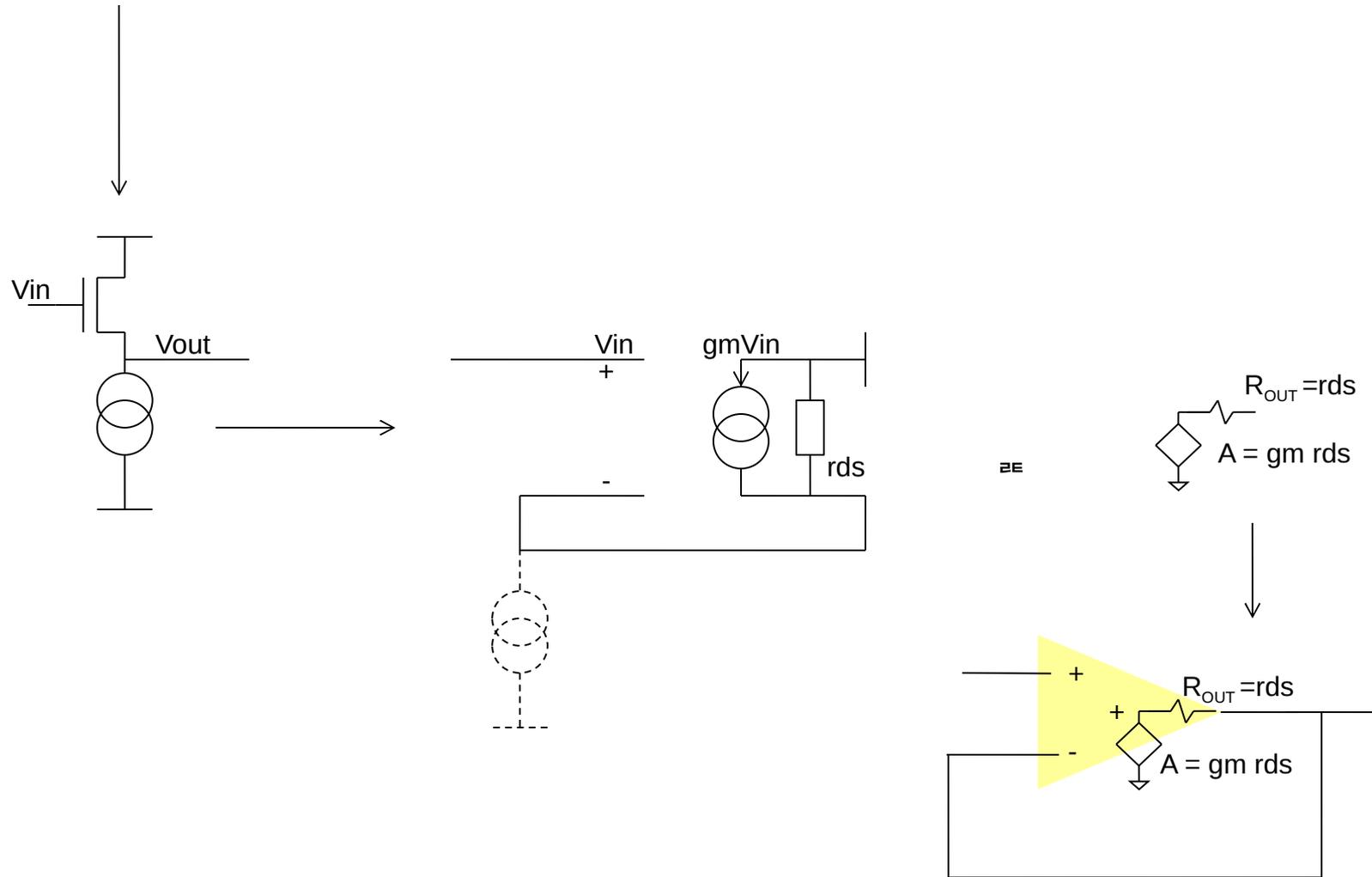
Verstärker mit zwei Stufen

Source-Follower als Ausgangsstufe

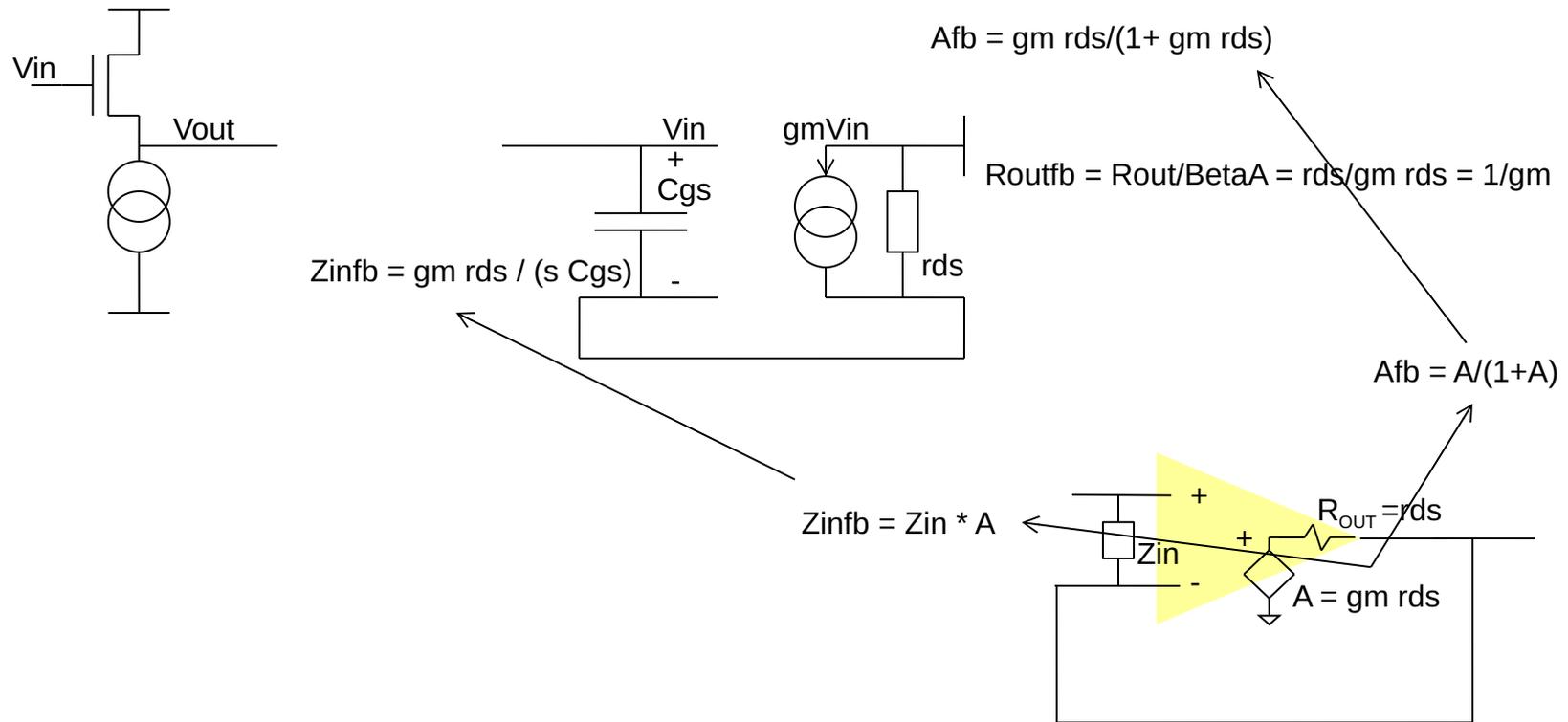
- Nichtinvertierender Verstärker (Buffer) als Ausgangsstufe
- Große Eingangsimpedanz Z_{in2} und kleine Ausgangsimpedanz Z_{out2}
- Schneller, R_{out} klein



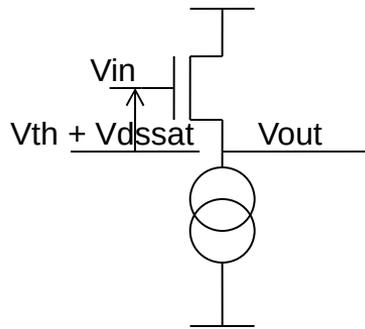
- Sourcefolger (Common Drain)



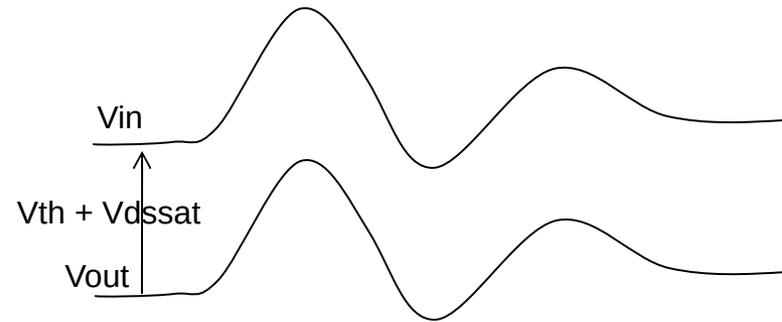
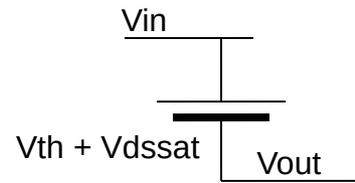
- Kleinsignalmodell



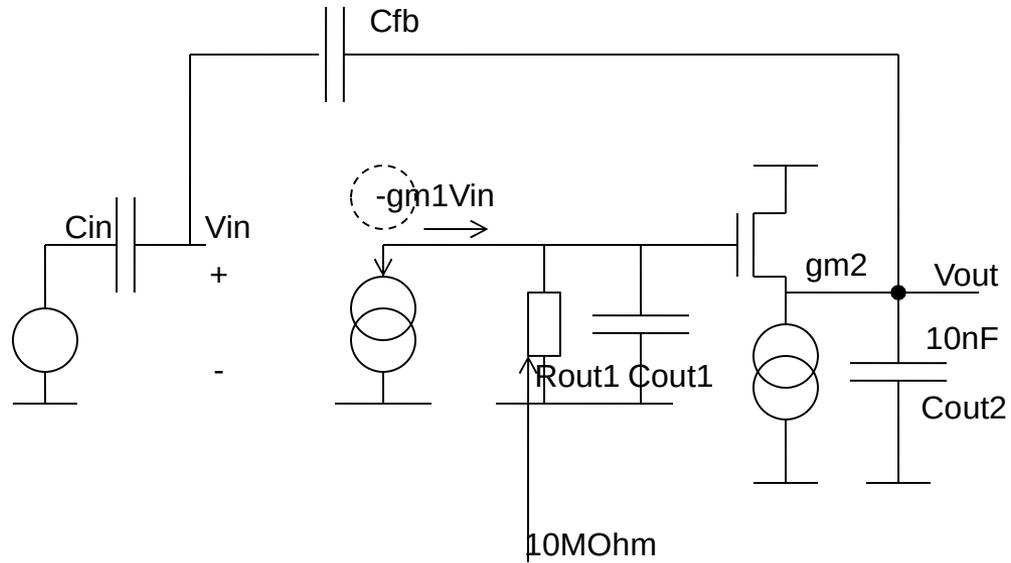
- Großsignalmodell



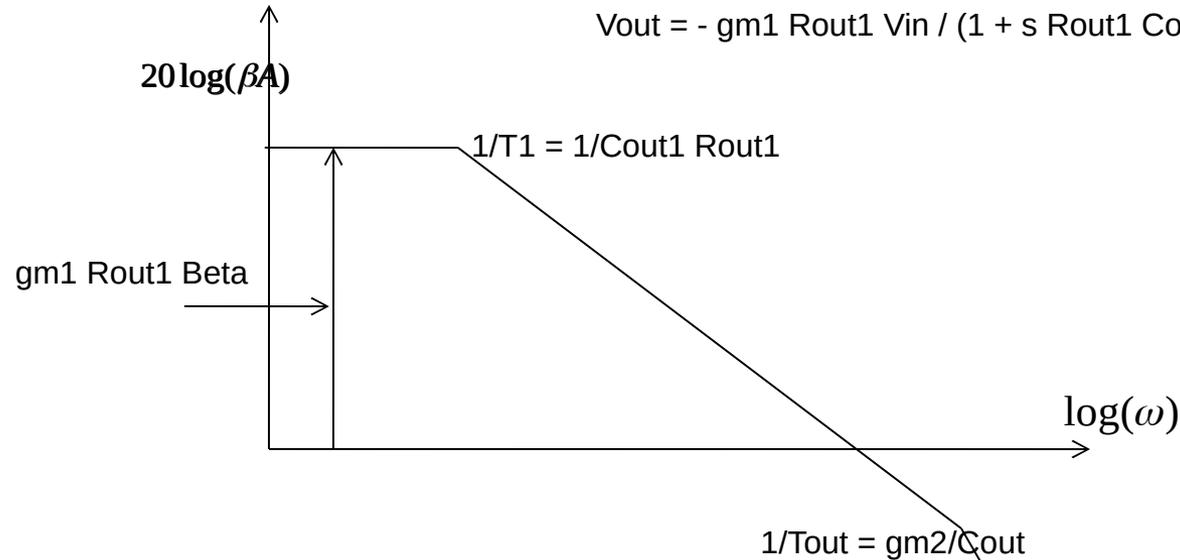
≅



- $T_{fb} = ?$

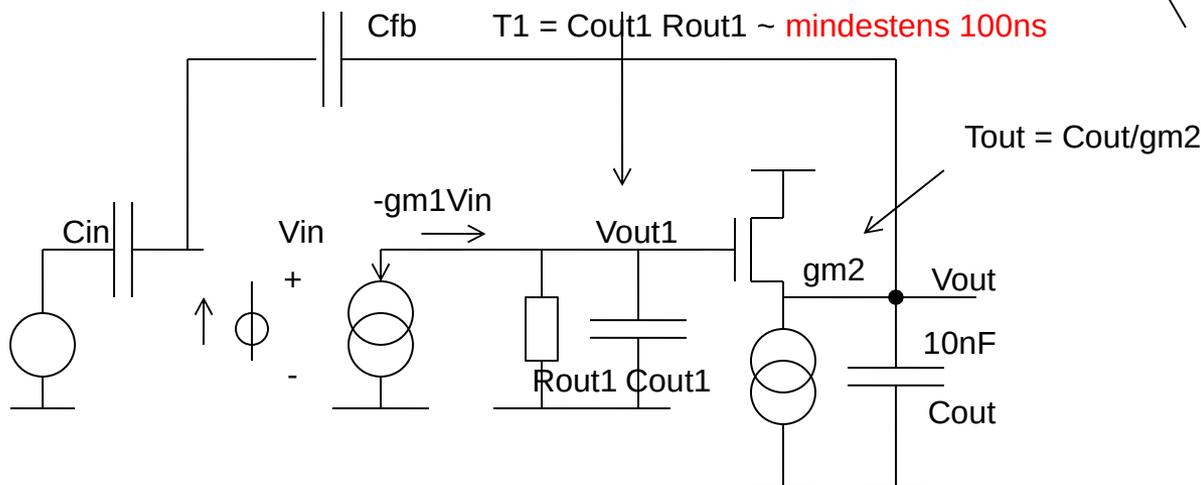


- Schleifenverstärkung hat zwei Zeitkonstanten

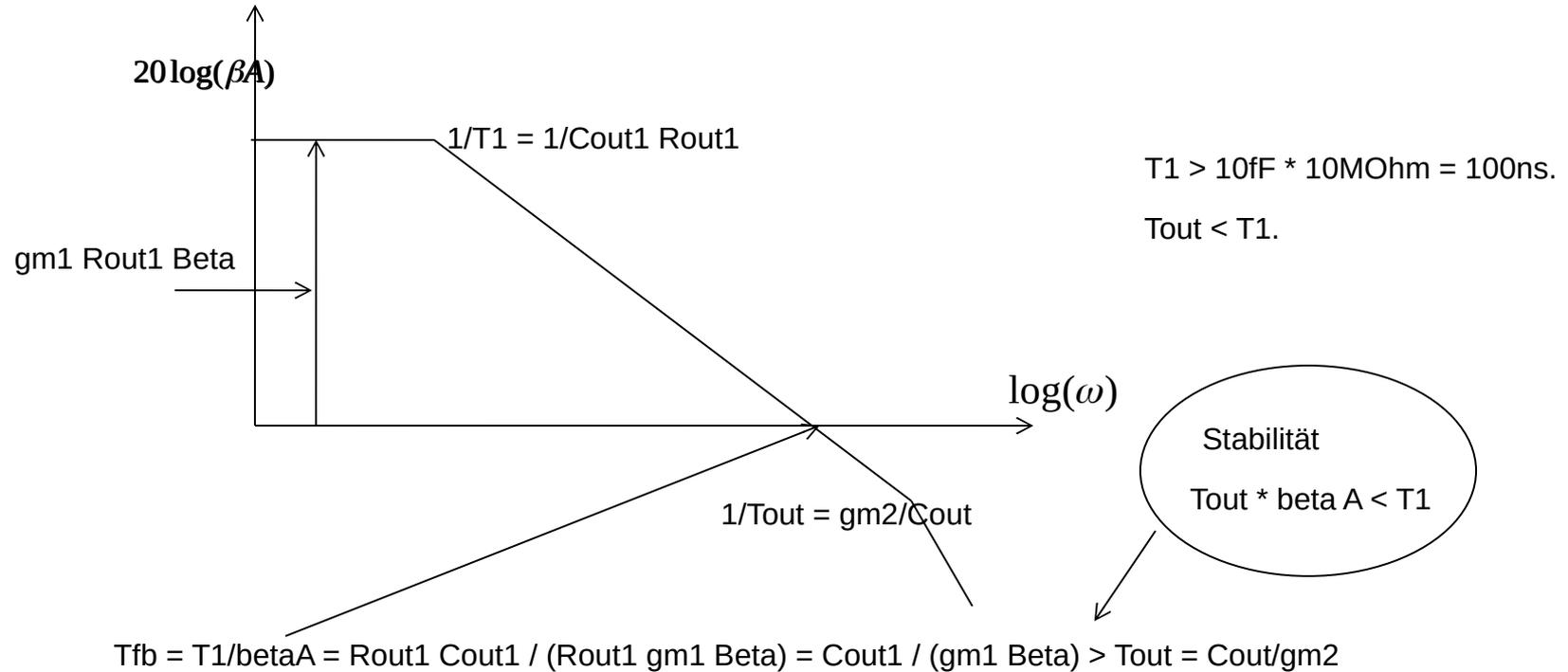


$T_1 > 10\text{fF} * 10\text{M}\Omega = 100\text{ns}$.

$T_{out} < T_1$.



- Stabilität



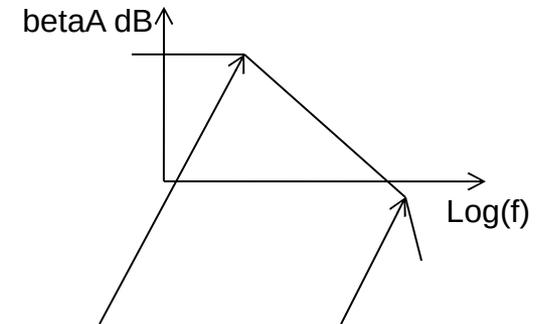
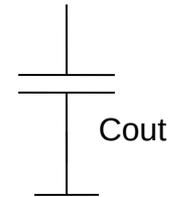
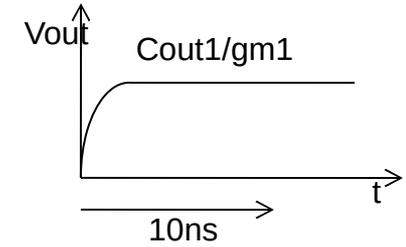
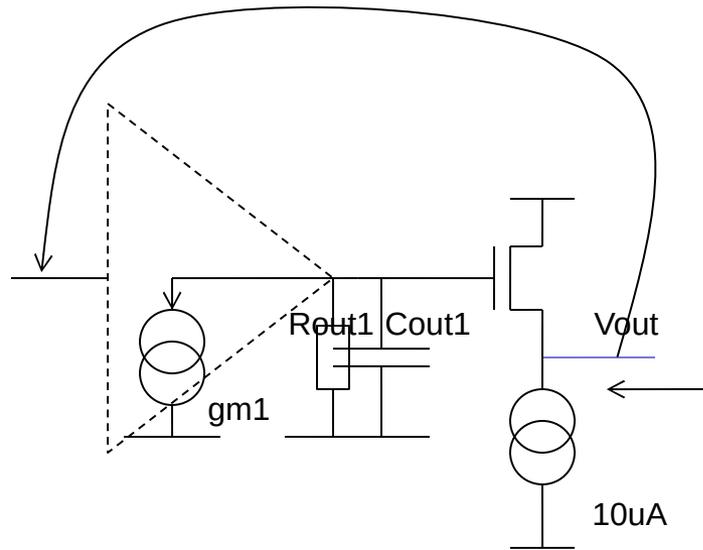
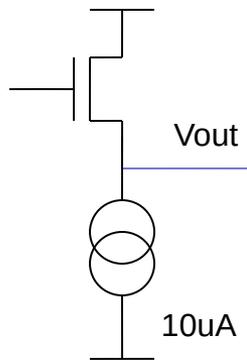
$T_{fb} = 10 \text{ns} \rightarrow C_{out}/gm_2 < 10 \text{ns}, \text{ oder } gm_2 > 10 \text{pF}/10 \text{ns} = 1 \text{mS}$

$T_{fb} = C_{out1}/gm_1 \beta \neq f(C_{out})$

Stabilität: $T_{out} = C_{out}/gm_2 < T_{fb}$

- Dimensionierung

$L = 200\text{n}$, $V_{dssat} = 100\text{mV}$, $W=?$

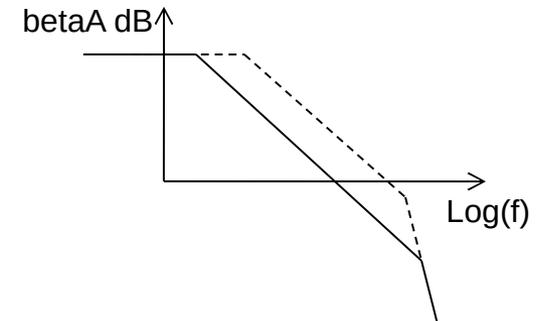
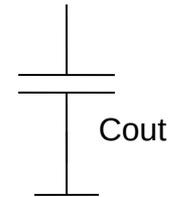
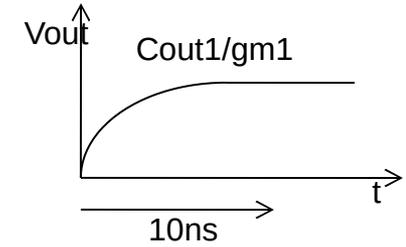
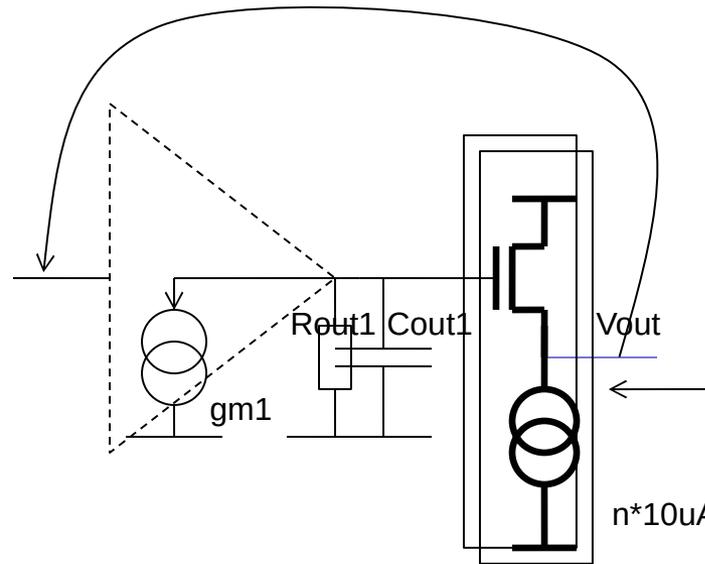
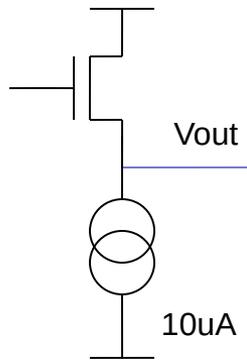


$1/T1 = 1/Cout1 Rout1$

$1/Tout = gm2/Cout$

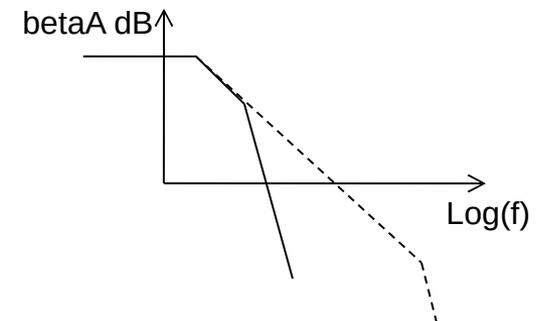
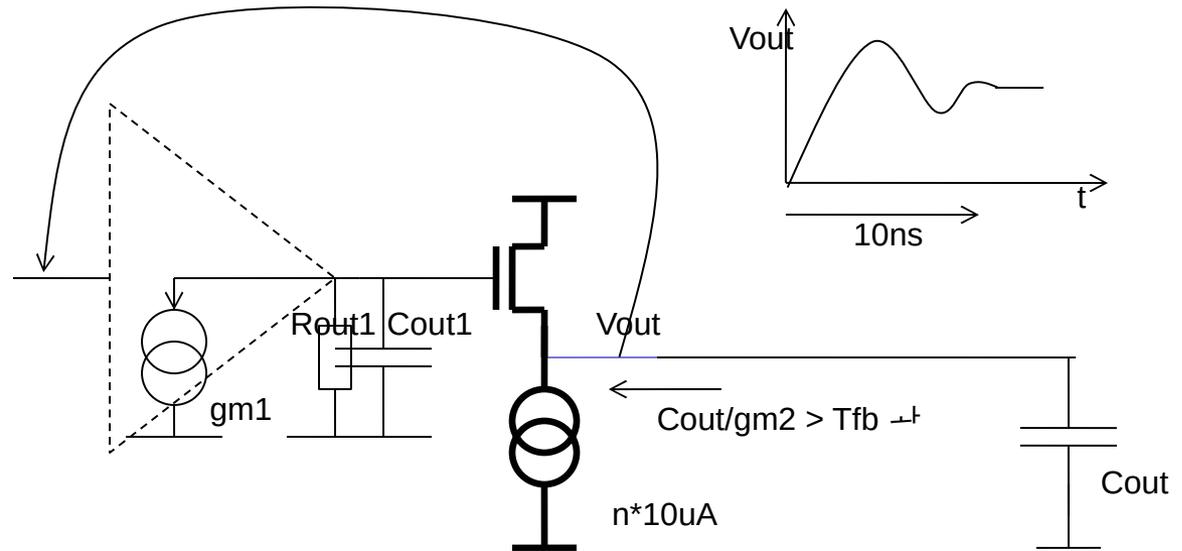
- Dimensionierung

$L = 200\text{n}$, $V_{\text{dssat}} = 100\text{mV}$, $W=?$



$$1/T_1 = 1/C_{\text{out}1} R_{\text{out}1} \quad 1/T_{\text{out}} = g_{m2}/C_{\text{out}}$$

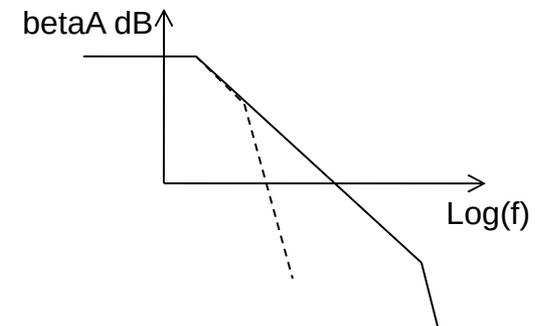
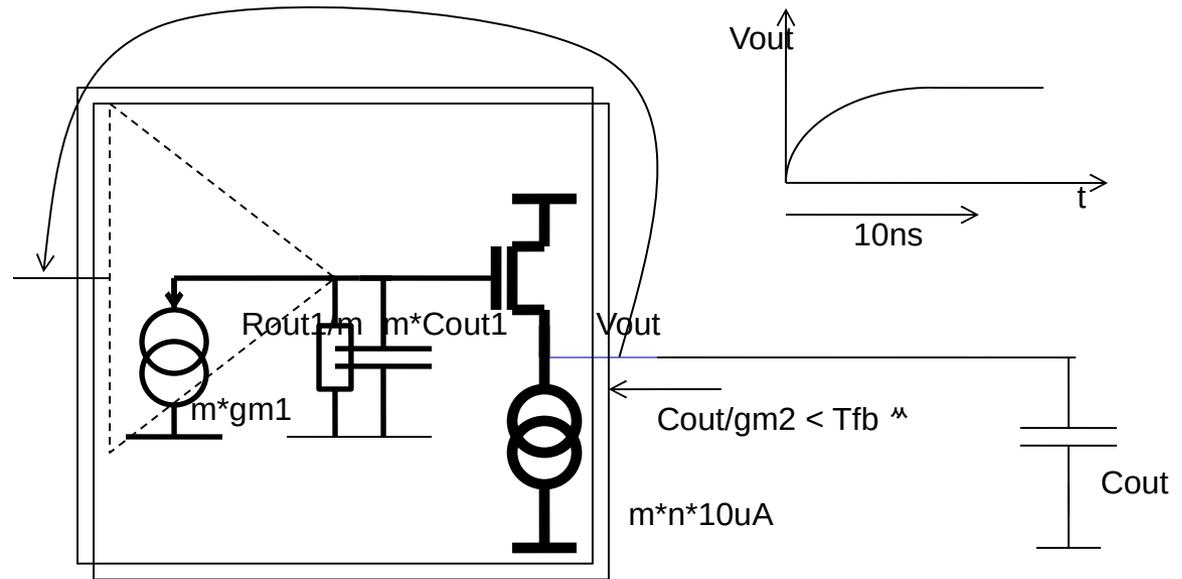
- Dimensionierung



$$1/T_1 = 1/C_{out1} R_{out1}$$

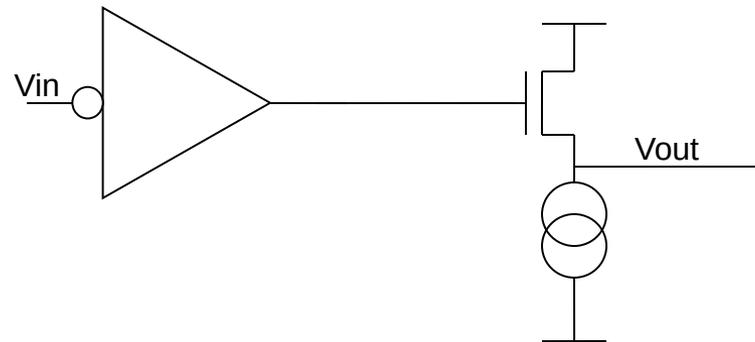
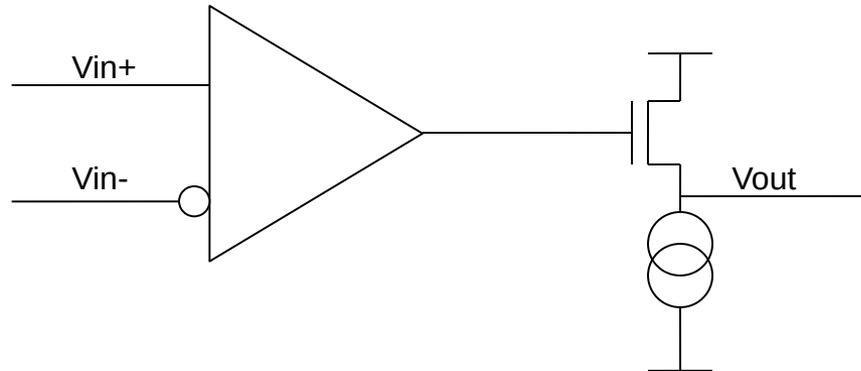
$$1/T_{out} = gm2/C_{out}$$

- Dimensionierung

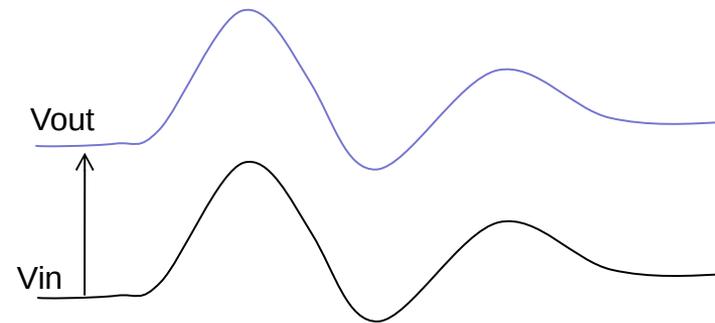
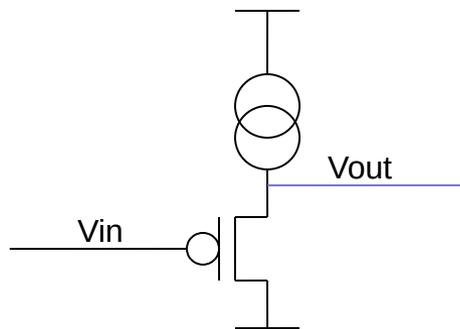
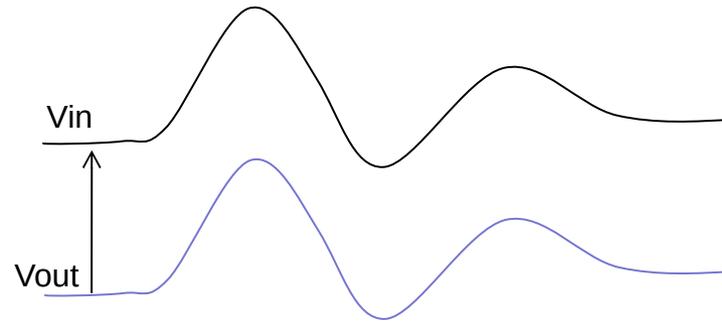
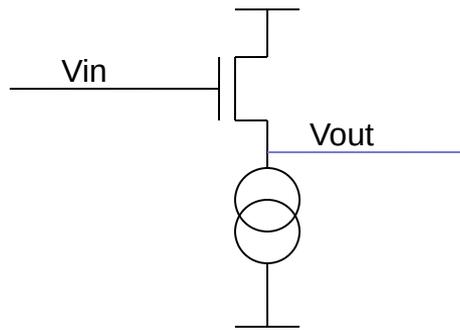


$$1/T_1 = 1/C_{out1} R_{out1} \quad 1/T_{out} = g_{m2}/C_{out}$$

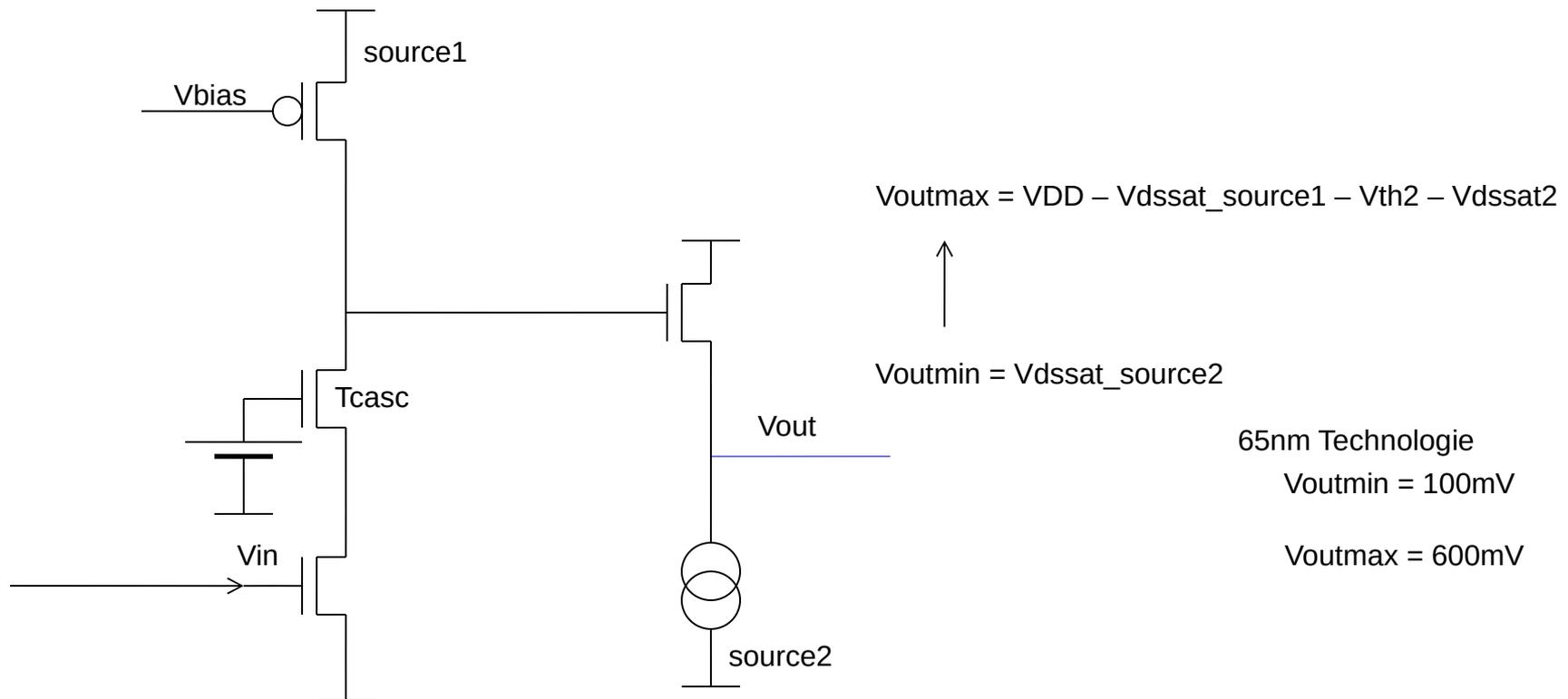
- Varianten



- Varianten

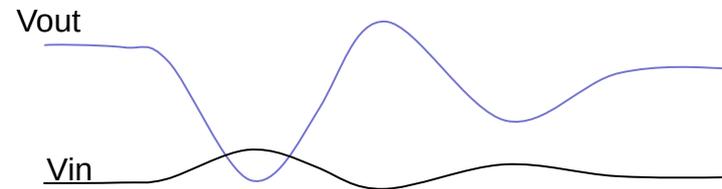
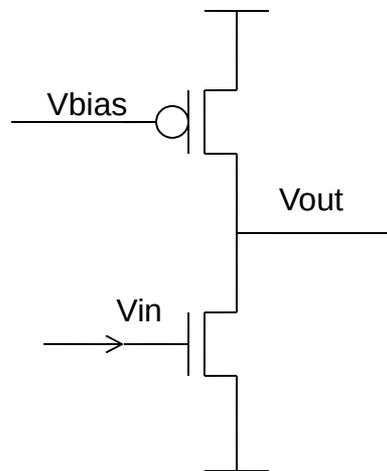


- Nachteile
- Keine Spannungsverstärkung in der zweiten Stufe, Rauschen
- Eingeschränkter Signalbereich



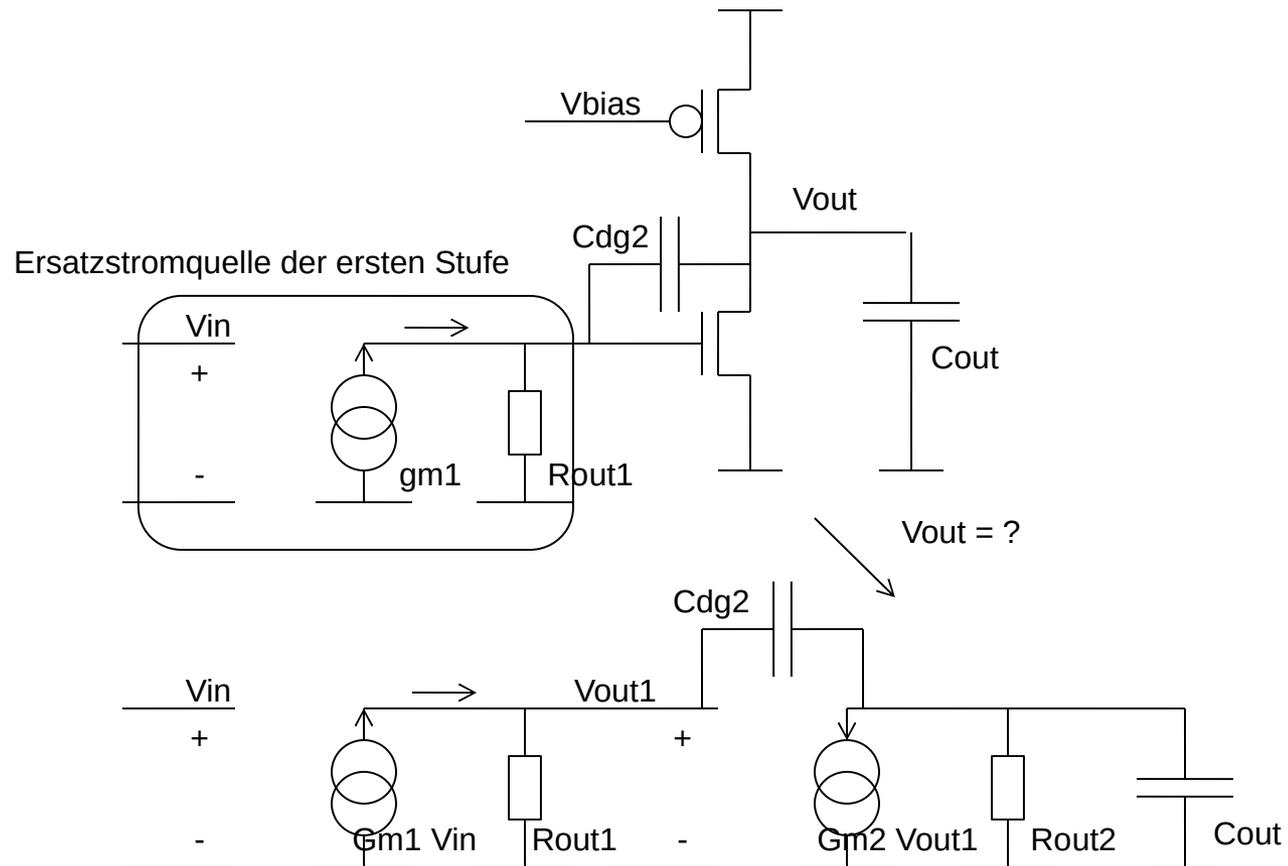
Verstärker mit zwei Stufen Common-Source als Ausgangsstufe

- Common Source Verstärker



$$A = -g_m R_{out}$$

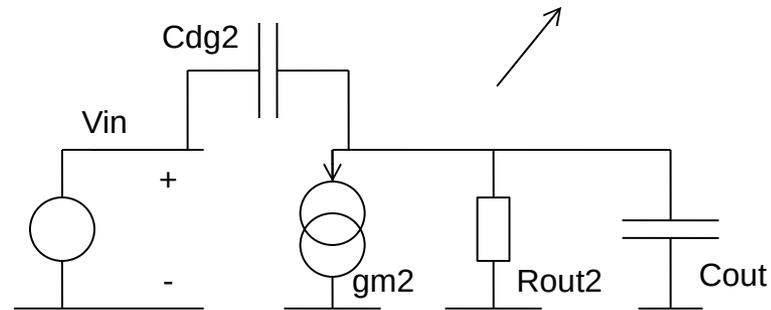
- Zweistufiger Verstärker



- Zweistufiger Verstärker

Vorlesung 9

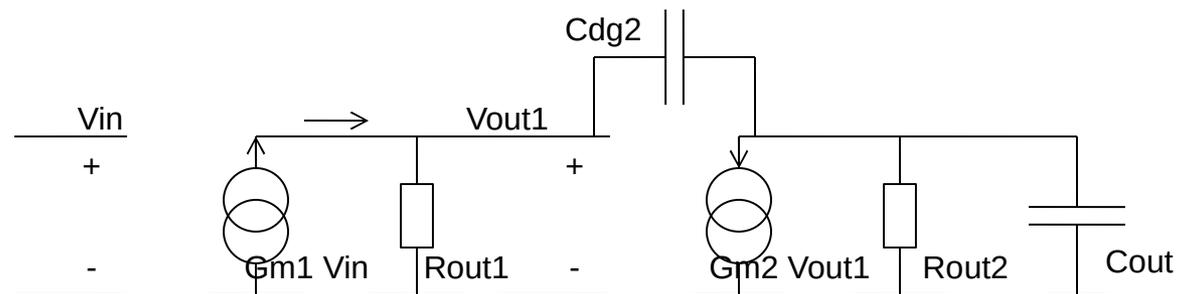
$$V_{out} = -g_{m2} R_{out2} (1 - s C_{dg2}/g_{m2}) V_{in} / (1 + s R_{out2} C_{out})$$



Vorlesung 10

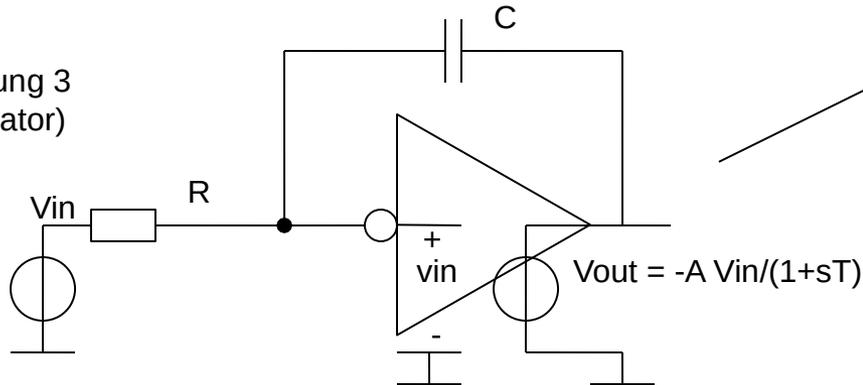
!=

Vout = ?



- Zweistufiger Verstärker

Vorlesung 3
(Integrator)

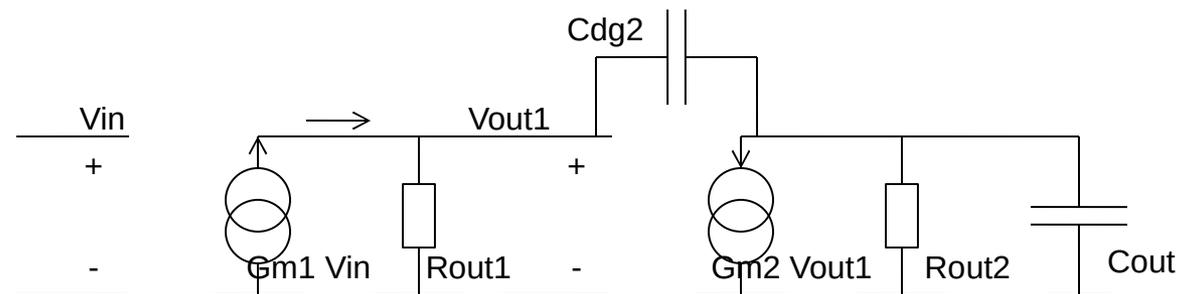


$$V_{out} = -A/(1 + s ARC)(1 + sT/A) V_{in}$$

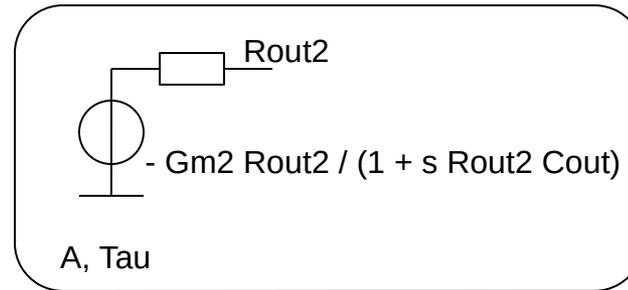
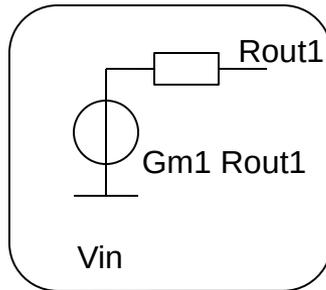
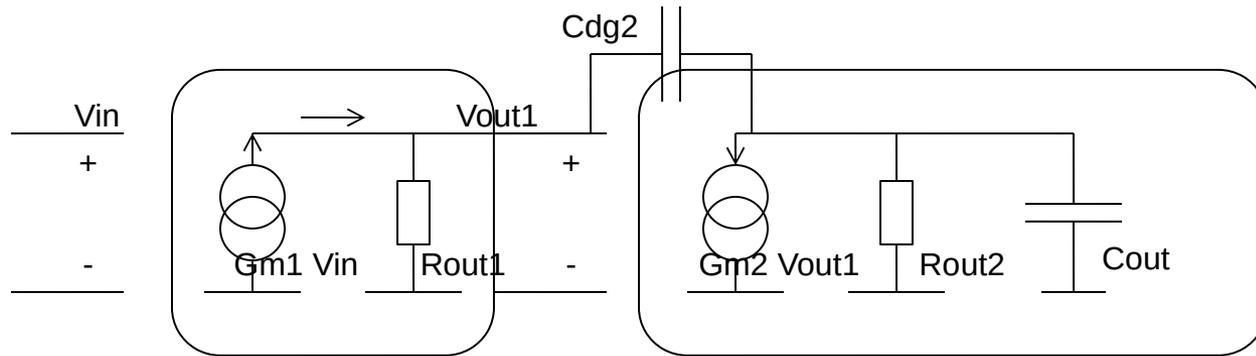
EE

Vout = ?

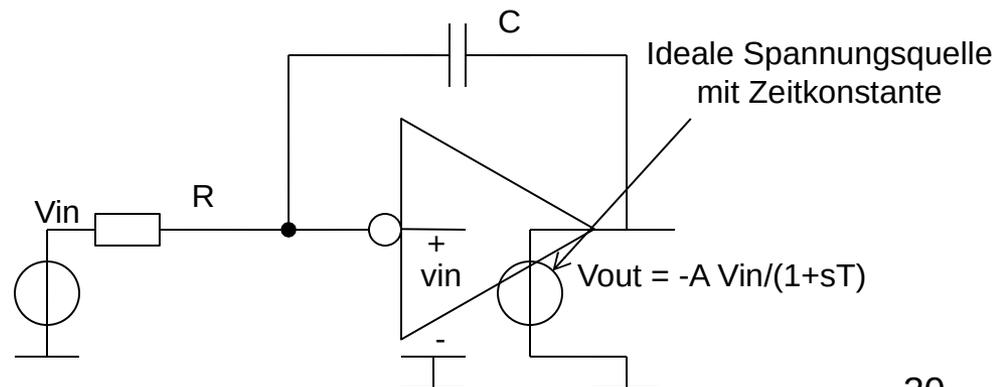
Vorlesung 10



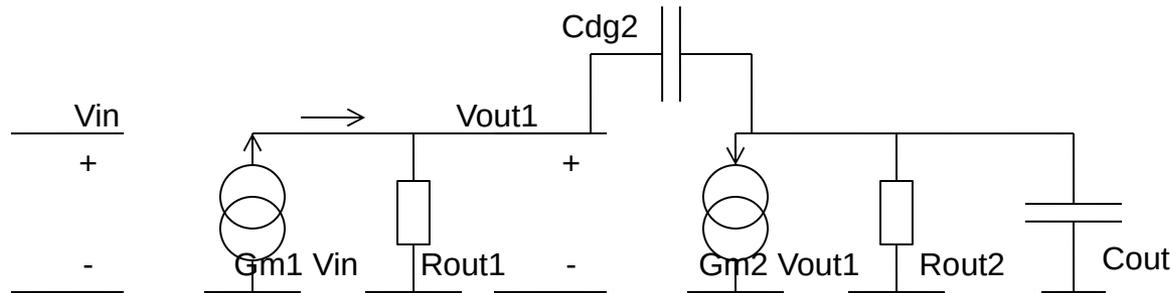
- Zweistufiger Verstärker



$R = R_{out1}$	$A = g_{m2} R_{out2}$
$V_{in} = g_{m1} R_{out1}$	$T = R_{out2} C_{out}$
$C = C_{dg2}$	



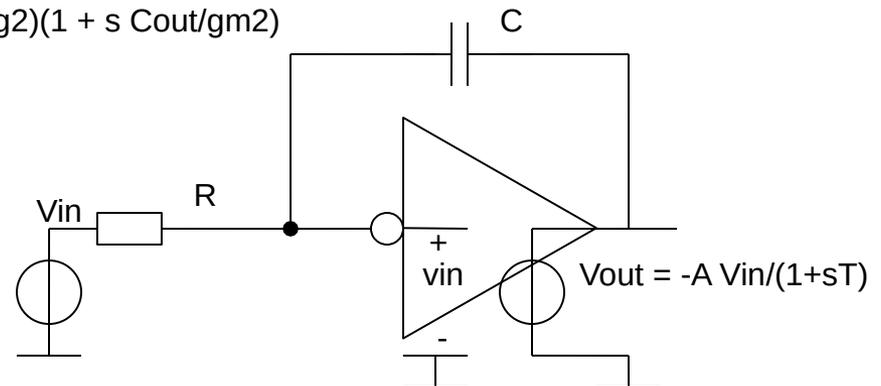
- Zweistufiger Verstärker



$R = R_{out1}$	$A = g_{m2} R_{out2}$
$V_{in} = g_{m1} R_{out1}$	$T = R_{out2} C_{out}$
$C = C_{dg2}$	

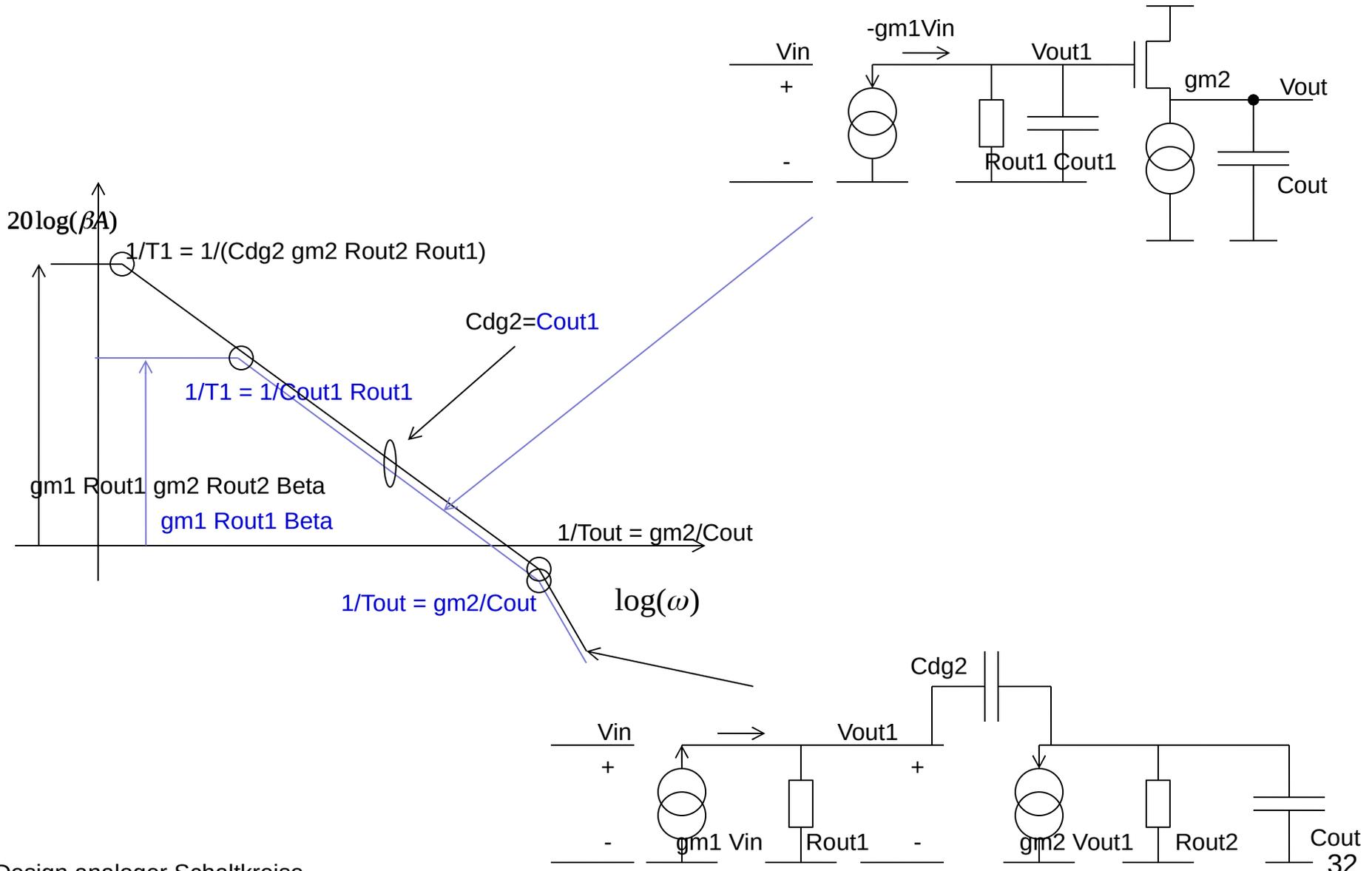
$$V_{out} = -A / (1 + s A R C) (1 + s T / A) V_{in}$$

$$V_{out} = -g_{m1} R_{out1} g_{m2} R_{out2} / (1 + s R_{out1} g_{m2} R_{out2} C_{dg2}) (1 + s C_{out} / g_{m2})$$

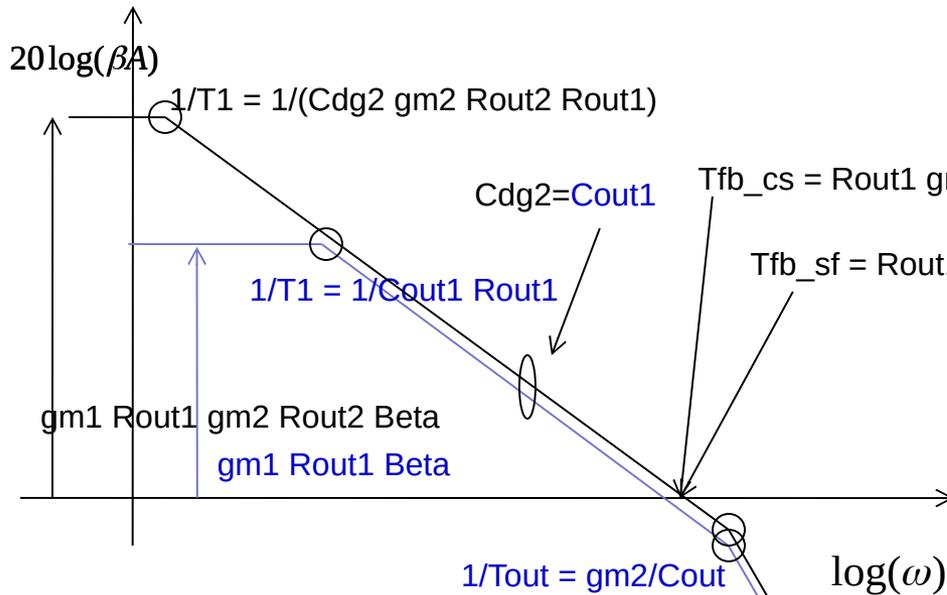
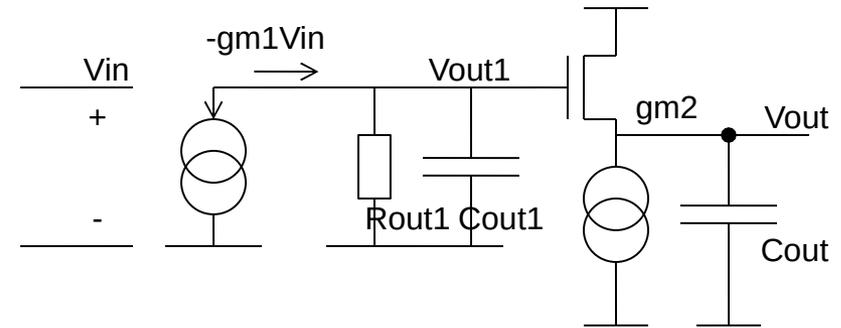


Vergleich: Sourcefolger, Common-Source

- Vergleich: Sourcefolger, Common-Source

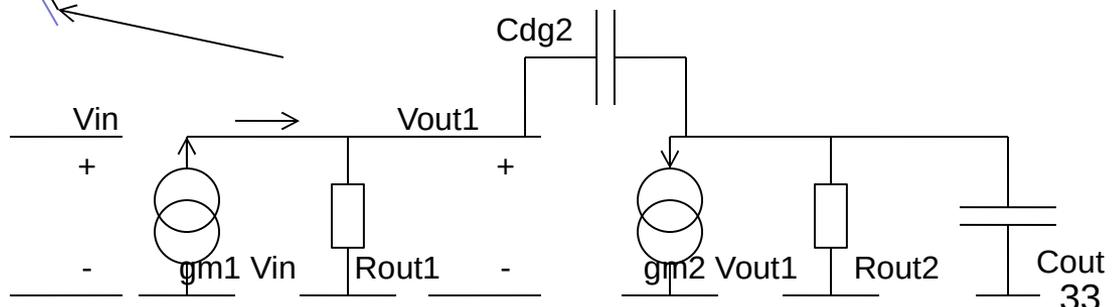


Vergleich: Sourcefolger, Common-Source

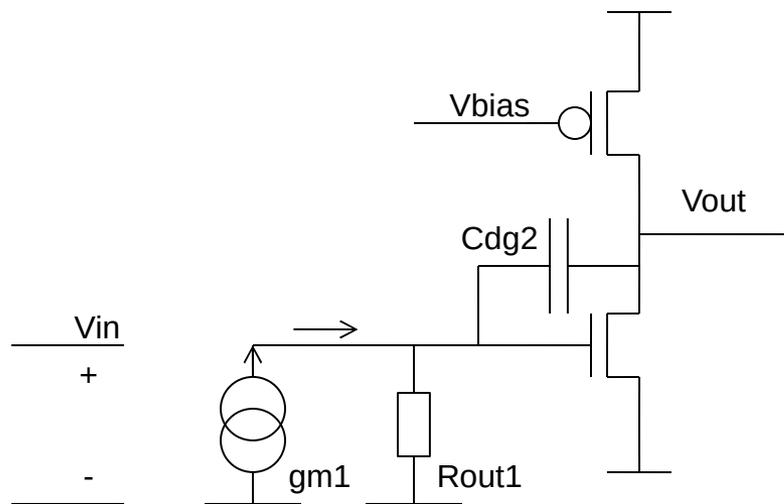


$T_{fb_cs} = R_{out1} g_{m2} R_{out2} C_{dg2} / (\beta g_{m1} R_{out1} g_{m2} R_{out2}) = C_{dg2}/g_{m1}$
 $T_{fb_sf} = R_{out1} C_{out1} / (\beta g_{m1} R_{out1}) = C_{out1}/g_{m1}$

$R_{outfb} = 1/(g_{m1} R_{out1} g_{m2})$



- Beide Schaltungen sind stabil und gleich schnell.
- Beide Verstärker haben sehr niedrigen Ausgangswiderstand $\sim 1 \text{ Ohm}$.
- Der Verstärker mit der Common-Source Ausgangsstufe hat um Faktor $g_{m2} R_{out2}$ höhere DC Verstärkung. Das ist wichtig wenn wir eine hohe Afb-Verstärkung (Verstärkung mit Gegenkopplung) realisieren wollen – die Linearität ist besser.
- Der Signalbereich am Ausgang ist ebenfalls besser.



$$V_{outmin} = V_{dssat_2}$$

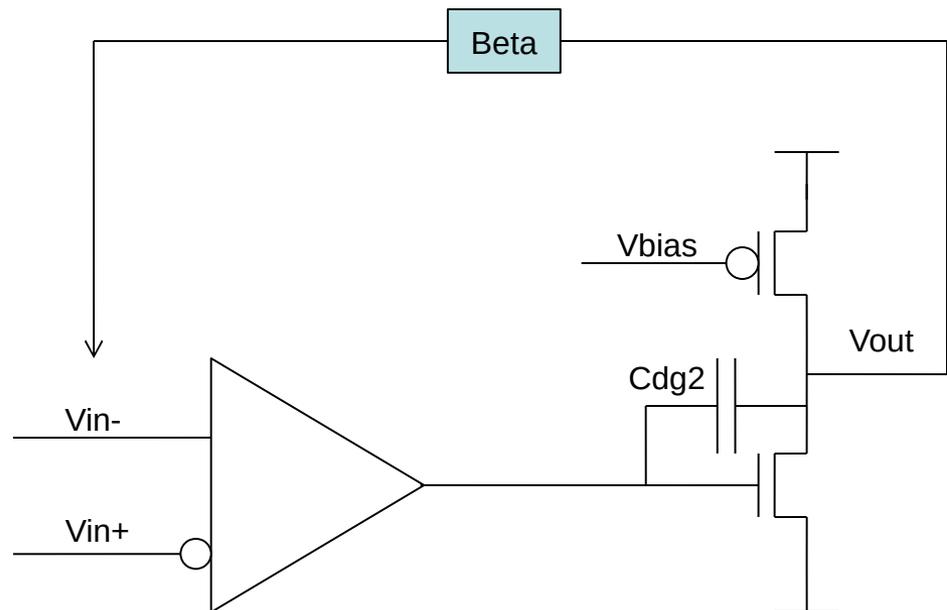
$$V_{outmax} = V_{DD} - V_{dssat_source2}$$

65nm Technologie

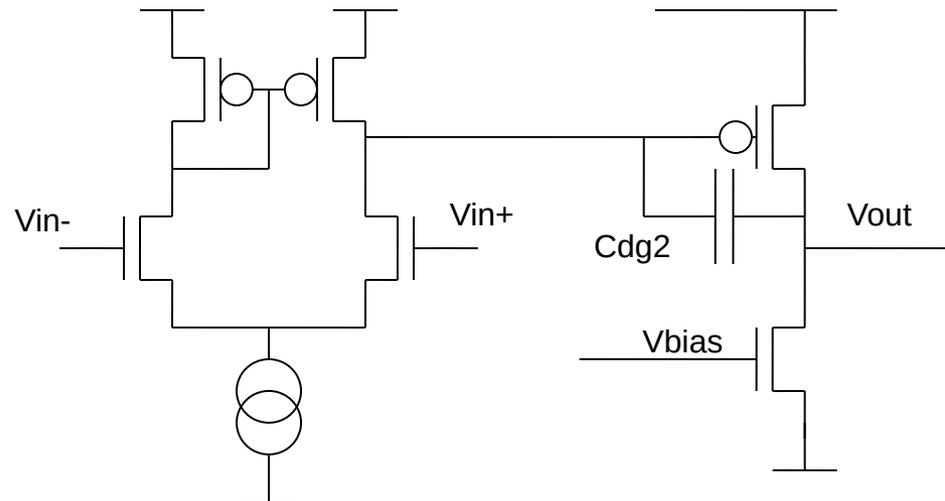
$$V_{outmin} = 100\text{mV}$$

$$V_{outmax} = 1.2 - 100\text{mV} = 1.1\text{V}$$

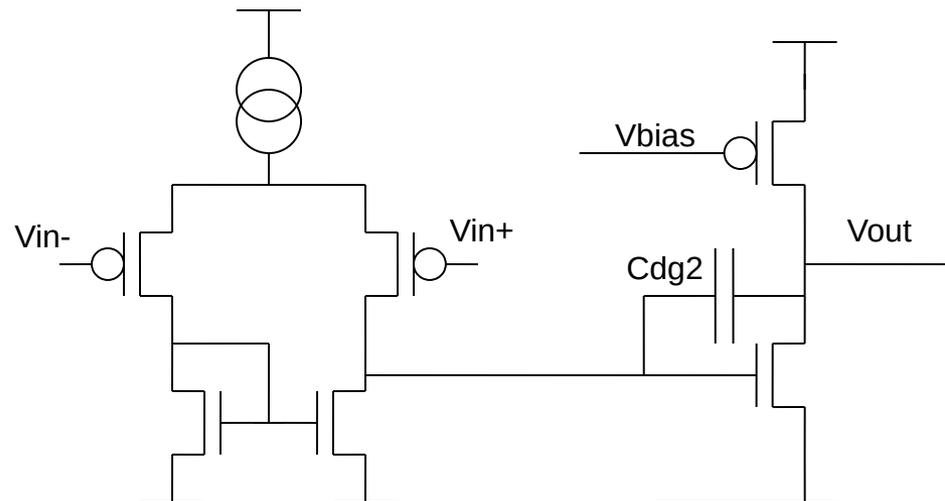
- Nachteil:
- Um eine Gegenkopplung zu realisieren muss entweder die erste Stufe eine positive Verstärkung haben, oder das Netzwerk für Rückkopplung eine negative Verstärkung



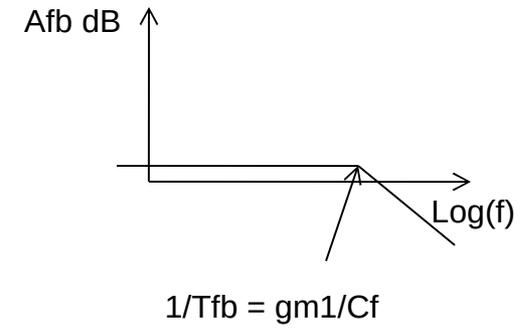
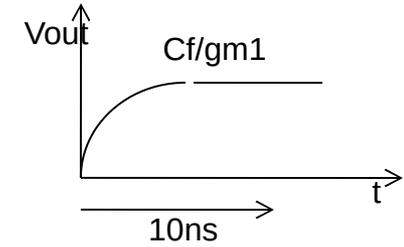
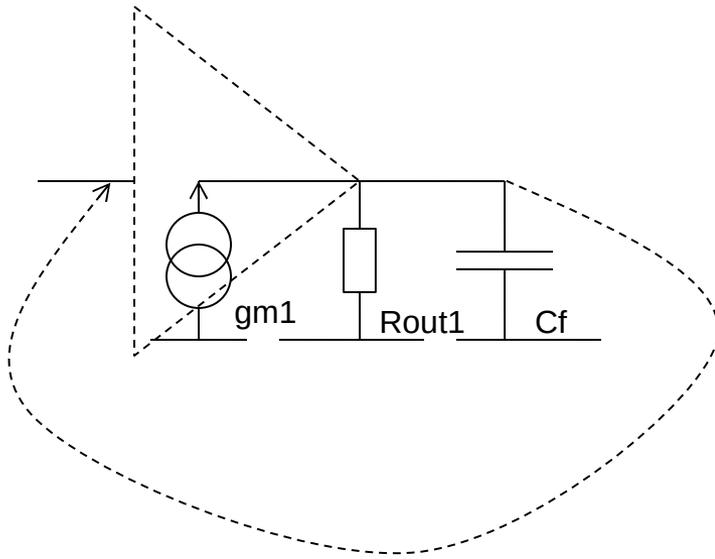
- Realisierung mit einem Differenzverstärker als 1. Stufe
- NMOS Variante



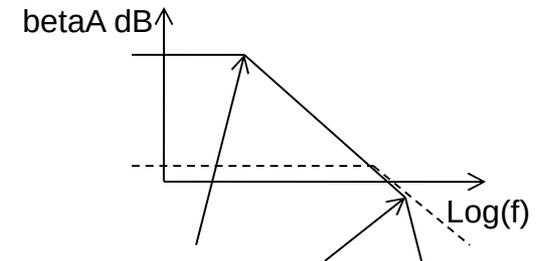
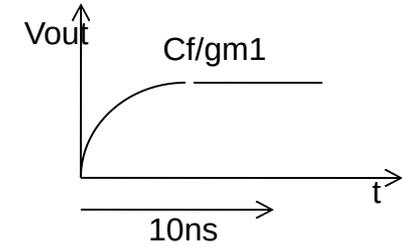
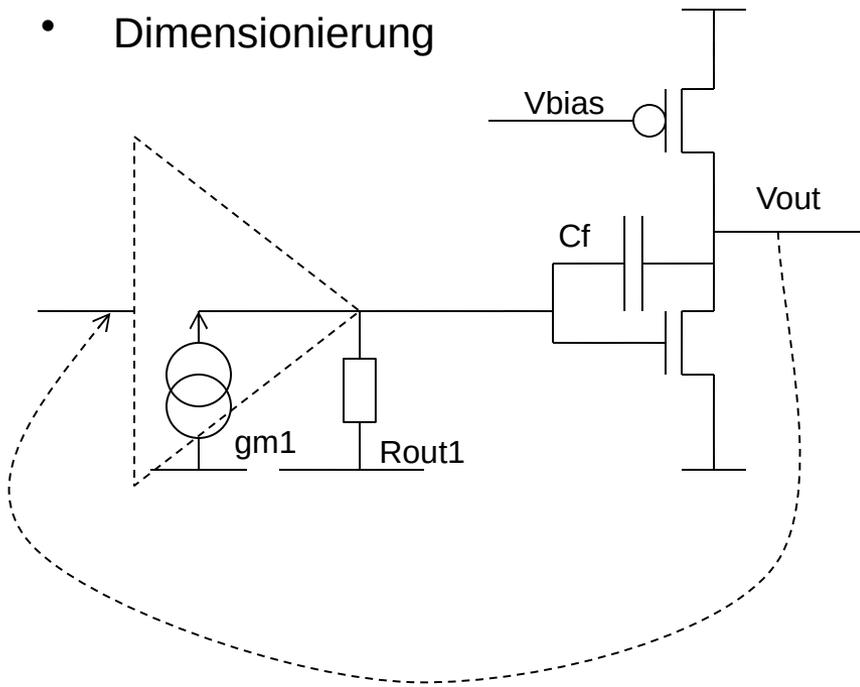
- Realisierung mit einem Differenzverstärker als 1. Stufe
- PMOS Variante



- Dimensionierung

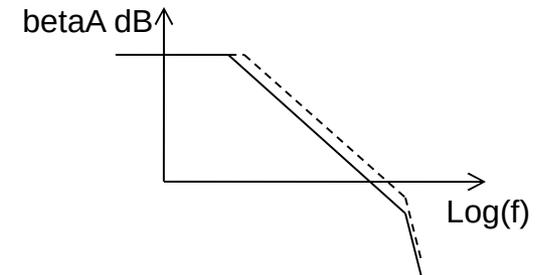
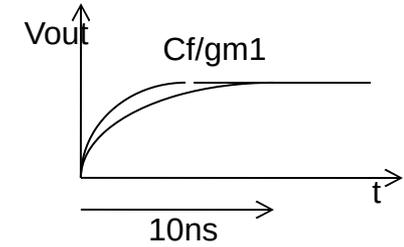
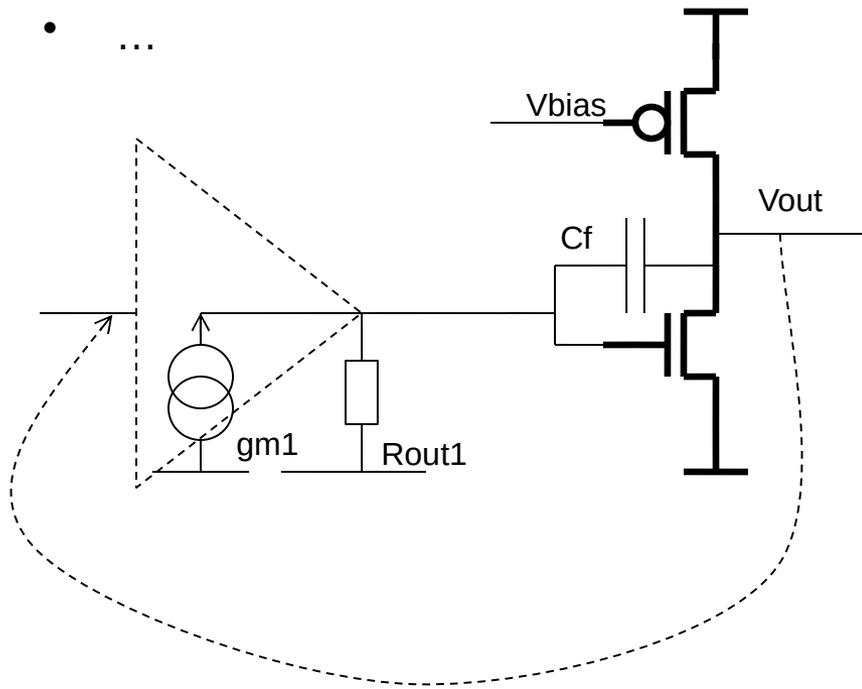


- Dimensionierung



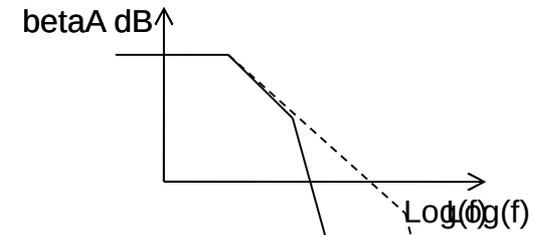
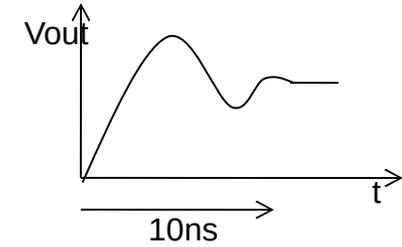
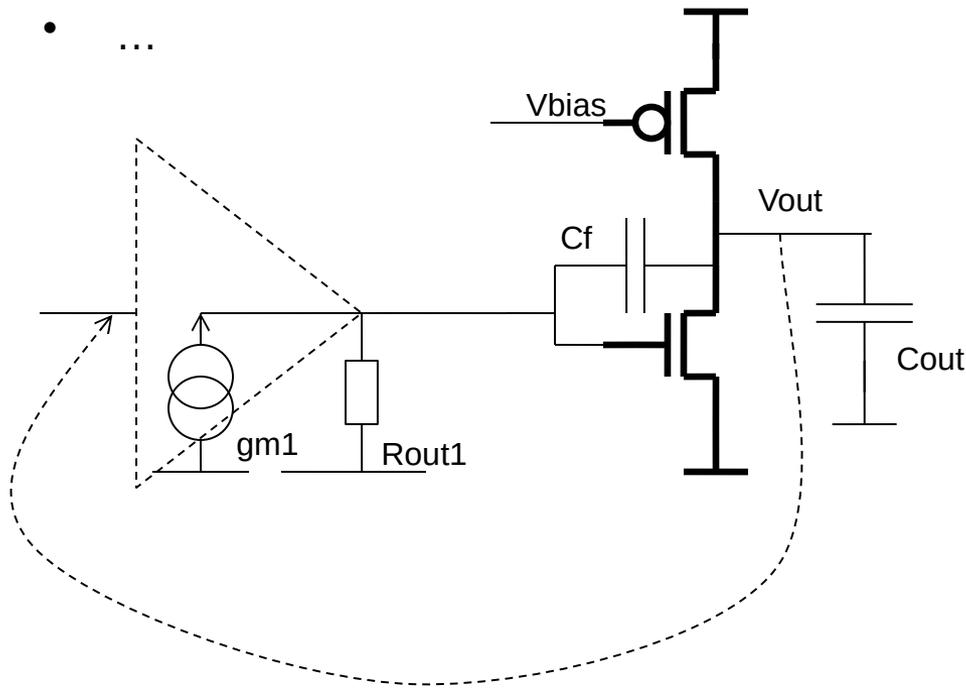
$$1/T1 = 1/Cf A2 Rout1$$

$$1/Tout = gm2/Cout$$



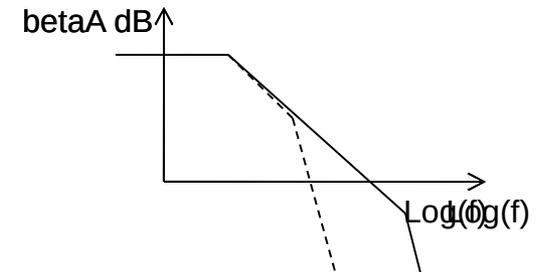
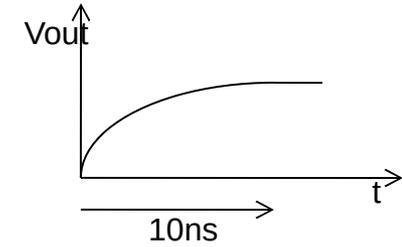
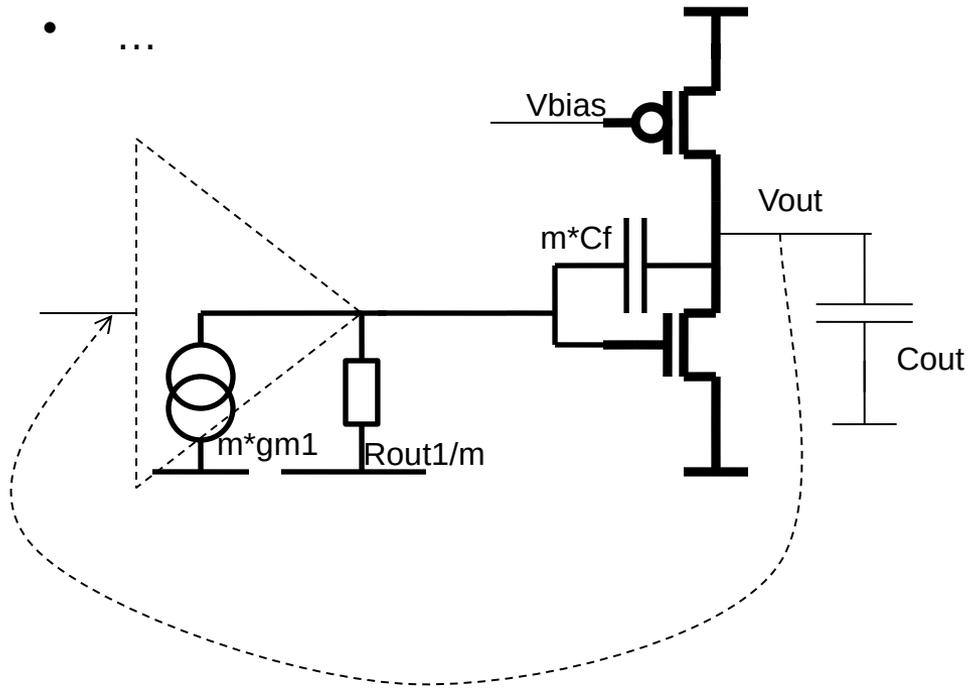
$$1/T_1 = 1/C_f A_2 R_{out1}$$

$$1/T_{out} = g_{m2}/C_{out}$$



$$1/T_1 = 1/C_f A_2 R_{out1}$$

$$1/T_{out} = g_{m2}/C_{out}$$



$$1/T_1 = 1/C_f A_2 R_{out1}$$

$$1/T_{out} = g_{m2}/C_{out}$$